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(19) (CA) **CANADIAN PATENT** (12)

(54) Silicate Treatment of Impure Silica Sands

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U.S.A.

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3 SILICATE TREATMENT OF
4 IMPURE SILICA SANDS
5
67 FIELD OF THE INVENTION
89 This invention relates to silica-containing foundry
10 sand and to a process for treating silica-containing foundry
11 sand with an alkali metal silicate to improve the tensile
12 strength of foundry cores or molds made from the sand.13
14 BACKGROUND OF THE INVENTION15 In the foundry art, cores or molds for making metal
16 castings are normally prepared from a mixture of an aggregate
17 material, such as sand, and a binding amount of a binder or
18 binder system. Typically, after the aggregate material and
19 binder have been mixed, the resulting mixture is rammed,
20 blown or otherwise formed to the desired shape or pattern
21 and then cured with the use of catalysts and/or heat to a
22 solid, cured state.23
24 A variety of different processes for forming molds
25 and cores have been developed in the foundry industry. One
26 type of process known as the shell molding process, is well
27 known in the art. While there are many variations of this
28

1 process, the process essentially comprises depositing a
2 combination of sand and potentially thermosetting resin
3 against a heated pattern such that the resin melts and
4 cures to form a rigid shell mold or core section for use
5 in the casting of metals. The combination of resin and
6 sand used in the process can be a mixture of powdered resin
7 and sand, or a free-flowing coated sand in which each grain
8 is coated with a nontacky layer of resin.

The production of a core or mold by the shell process involves two basic steps, the invest and the cure step. In the first step, the resin-coated sand is dumped onto or blown against the heated metal pattern. The resin-coated sand is held against the pattern (invested) until the shell is thick enough to hold metal in a given application. In the second step, the resin-coated sand is dumped or dropped away from the shell of bonded coated particles of sand and the resulting shell is cured. After the shell is cured, it is removed from the hot metal pattern and is ready for use.

Another process, known to the art as the "no-bake" process, is also used in forming resin cores. This process requires no external heating. Instead, curing is accomplished by means of a catalyst added just before the sand and resin components are introduced into the core box. Base-cured resin components used in the no-bake process are generally

1 mixtures of polyols and polyisocyanates. Solutions of these
2 components are usually coated on the sand immediately before
3 use.

4
5 A third process for making cores and molds employs
6 sands treated with core oil mixes. These mixes contain drying
7 oils and cereal binders. Cores and molds made with such core
8 oil mixes are cured by baking them in an oven.

9
10 In all of these processes, the binder which has been
11 mixed with sand acts, when cured, to bind the particles of sand
12 in the form of the pattern. The core or mold must be strong
13 enough to contain the molten metal until it solidifies. For
14 this reason, a core or mold with high tensile strength is
15 required.

16
17 One factor influencing the tensile strength of the
18 cores and molds is the quality of the sand used in their
19 preparation. When a silica sand is employed, it is generally
20 necessary to use a sand of high purity. In the past, when
21 silica sands of lower purity were used, it was necessary to
22 add large amounts of binder to ensure structural integrity
23 of the mold. This was not only costly but led to other
24 undesirable results when gaseous decomposition products of
25 the excess resin penetrated into the molten or solidifying
26 metal resulting in pinholes and scarring of the metal shape.

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1 Impure silica sands, such as lake and bank sands,
2 are readily available in many areas of the United States.
3 These impure sands are sometimes beneficiated by various
4 processes such as water washing. However, it is still
5 necessary to use excess binder with the washed sands to
6 obtain the desired tensile strength of the cores and molds
7 made from them. It is therefore desirable to develop a
8 process whereby these inexpensive sands can be used to make
9 foundry cores and molds without the need to use excess binder
10 with the sand.

11
12 Bushey described a method for treating zircon-
13 containing sands, U.S. Patent 4,115,345, and olivine sands,
14 U.S. Patent 4,154,894, with an alkali metal silicate to
15 improve the tensile strengths of resin shell molds or
16 cores made from the sands. However, he reported that when
17 this method was used with silica and chromite sands, no
18 improvement in the tensile strength of the cores and molds
19 was observed.

20
21 A process has now been discovered which permits
22 the use of impure silica sands in conjunction with moderate
23 amounts of binder to form foundry cores and molds with
24 improved tensile strength. This process is less expensive
25 than present beneficiation methods and gives cores and molds
26 with improved tensile strengths.

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1 A further unexpected benefit of using these treated
2 sands is that cores prepared from them by the base-curing
3 "no-bake" process are more readily released from the core
4 box. Easy release of the cores is commercially important,
5 since sticking cores slow down the core-making process and
6 often become broken and useless.

7

- 8 SUMMARY OF THE INVENTION

9

10 In accordance with this invention, there is
11 provided a process for the preparation of treated silica
12 sand which is useful for forming foundry cores and molds
13 having improved tensile strength. The process comprises
14 treating an impure silica sand with an aqueous solution of
15 an alkali metal silicate and heating the mixture of sand
16 and silicate.

17

18 Additionally, in accordance with this invention,
19 there is provided a process for the preparation of a
20 molding composition useful for forming foundry cores and
21 molds having improved tensile strength. The process
22 comprises treating impure silica sand with an aqueous
23 solution of an alkali metal silicate and heating the
24 mixture of sand and silicate. The treated sand is then
25 mixed or coated with an effective bonding amount of a
26 binder selected from the group consisting of shell resins,
27 base-curing "no-bake" resin compounds and core oil mixes.

1 Furthermore, in accordance with this invention,
2 there is provided silica foundry sand useful for making
3 foundry cores and molds with improved tensile strength.
4 This is prepared by treating impure silica sand with an
5 aqueous solution of an alkali metal silicate and heating
6 the mixture of sand and silicate.

7
8 Finally, in accordance with this invention,
9 there is provided a molding composition useful for
10 preparing foundry cores and molds having improved tensile
11 strength. This composition comprises an impure silica
12 sand, which has been treated by heating with an aqueous
13 solution of an alkali metal silicate, and an effective
14 bonding amount of a binder. The binder is selected
15 from the group consisting of shell resins, base-curing
16 "no-bake" resin components and core oil mixes.

17
18 DETAILED DESCRIPTION OF THE INVENTION

19
20 Any impure silica sands may be used in the practice
21 of this invention. Examples of such sands are lake and bank
22 sands which generally consist of from about 85% to about 98%
23 by weight of silicon dioxide and small amounts of such
24 impurities as aluminum oxide, iron oxide, alkaline oxides
25 and alkaline earth oxides. The impure silica sand can be
26 a naturally-occurring silica sand or a mixture of various
27 silica sands. The processes of this invention are useful

1 if the sand or mixture of sands contain less than about
2 99% silicon dioxide.

3
4 Commercially available lake and bank silica sands
5 include 20KK Sand, available from the Martin Marietta
6 Corporation, Bridgman, Michigan; Ludington Sand, available
7 from the Sargent Sand Company, Saginaw, Michigan; Muskegon
8 Sand No. 850 and Beneficiated Muskegon Sand W/51, available
9 from the Nugent Sand Company, Muskegon, Michigan; and
10 Vassar Sand, available from the Sargent Sand Company,
11 Saginaw, Michigan.

12
13 In the process of this invention, the impure
14 silica sand is treated with an aqueous solution of an
15 alkali metal silicate. Treatment may be carried out by
16 stirring a slurry of the sand in a dilute silicate solution.
17 It is often satisfactory to treat the sand with a more
18 concentrated silicate solution by placing the sand in
19 a mixer and adding the required amount of silicate solution
20 to the sand with mixing. Alternatively, the silicate solution
21 may be sprayed onto a thin layer of the sand.

22
23 Any alkali metal silicate, such as sodium and
24 potassium silicate, can be employed in the process of this
25 invention. Solutions of sodium silicate are commercially
26 available. Such solutions contain varying ratios of
27 sodium oxide to silicon dioxide. These weight ratios may

1 vary from 1 to 4 parts of silicon dioxide per 1 part of
2 sodium oxide. The amount of water present in the alkali
3 metal silicate solution is not critical. However,
4 sufficient water should be present to permit adequate
5 dispersion of the silicate over the surface of the sand
6 grains.

7
8 The amount of alkali metal silicate used with a
9 given sand should be an amount that effectively imparts
10 the desired strength to the cores or molds without
11 interfering with the free-flowing properties of the
12 silicate-treated sand. It is preferred to use from about
13 0.2 to about 1.1 g of silicate on a dry solids basis per
14 kg of sand.

15
16 After the silica sand has been thoroughly mixed
17 with the silicate solution, the sand may be isolated from
18 the slurry by any conventional means such as decantation
19 or filtration. However, when the more concentrated
20 solutions of silicate are employed, no mechanical separation
21 of the sand from the silicate solution is required. It is
22 only necessary to heat the sand to about 100°C, or above,
23 for a short period of time to evaporate a portion of the
24 water and provide a free-flowing sand for use in the coating
25 process. This simplifies the process by avoiding a
26 decantation or filtration step.

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Alternatively, the sand can be preheated before the silicate solution is added to it. Mixing is then continued until the water is evaporated.

The silicate-treated silica sands of this invention 5 are used to make foundry molds or cores using the procedures practiced with pure silica sand. In general, these processes involve mixing the sand with effective bonding amounts of binders. Usually, the components of the binders are coated on the sand to insure their uniform distribution.

10 Details of the preparation and use of resin-coated sands in the shell molding process are given in U.S. Patent 3,838,095. Illustrative of "no-bake" processes, using base-curing polyurethane resin components, are U.S. Patents 3,409,579 and 3,429,848. The use of core oil mixtures as 15 foundry core binders is described in U.S. Patent 2,875,073.

Suitable resins for use in the shell-molding process include phenol-formaldehyde novolak resins which become thermosetting when heated in the presence of a curing agent. Hexamethylenetetramine is a satisfactory curing 20 agent for these resins. Single-stage phenol-formaldehyde shell resins which require no added curing

agent can also be used. Foundry sand, which has been coated or mixed with resin is placed in a mold and heated to cause the resin to harden forming a shell of resin-bonded sand. When the silicate-treated silica sand of this invention is used as the sand component in the mold, the resulting mold shows considerably improved tensile strength over the molds prepared using untreated impure silica sand at the same resin loading.

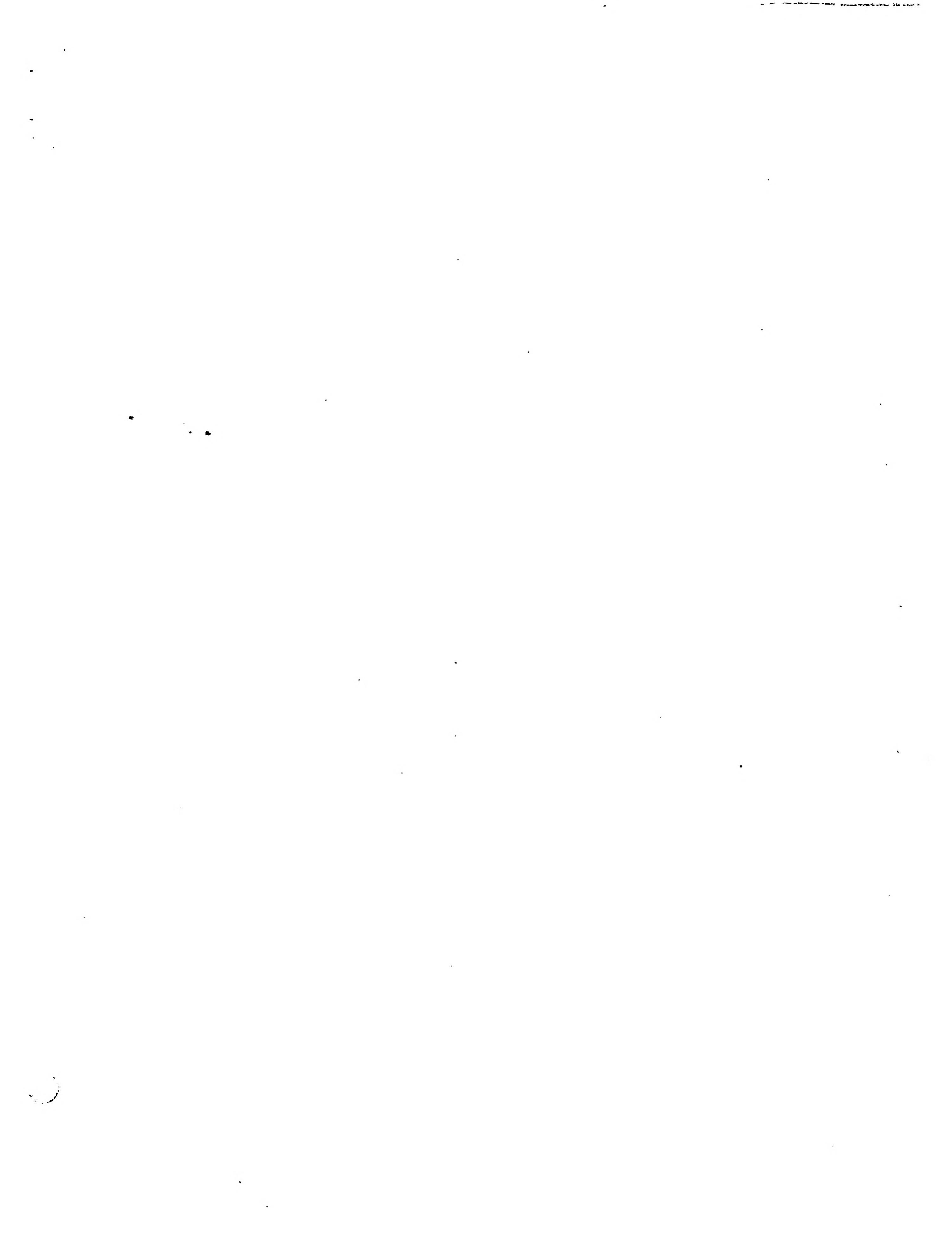
Resin components useful in the no-bake process are polyols and polyisocyanates. A variety of polyols can be used, but resole-type phenolic resins are often employed. These are usually dissolved in a solvent mixture and mixed with the sand. Polyisocyanates, either as liquids or in solution are also added. Then a basic catalyst is added to the mixture just before it is placed in the mold. It cures without heating. Tertiary amines are commonly used as the basic catalysts. When the silicate-treated silica sand of this invention is used in the base-catalyzed "no-bake" process, the resulting cores show better tensile strength and better scratch hardness than do cores prepared from untreated impure silica sand. Cores prepared from the treated sand are also easier to remove from the core box.

It is often the practice in the foundry art to include a variety of additives in the resins used to prepare foundry cores and molds. These additives include such materials as silanes, sources of fluoride, deodorizing agents and the like. Such additives may be used with resins in the present process and do not interfere with the improved tensile strength of the cores and molds obtained from the sands of this invention.

The following examples illustrate the invention. It is to be understood that the examples are illustrative only and do not intend to limit the invention in any way. In the examples, all parts and percentages are by weight and the temperatures are degrees centigrade unless otherwise indicated. All tensile strengths are given in pounds per square inch (psi).

EXAMPLE 1

An aqueous solution containing 2.8 g/l of sodium silicate was prepared by mixing with 10 l of water 73 g of a sodium silicate solution available from the Diamond Shamrock Corp., containing 9.1% by weight of Na_2O and 29.2% by weight of SiO_2 . Five kilograms of 20KK silica sand was added to the silicate solution and the mixture was stirred for 40 minutes. After stirring was stopped, the sand was allowed to settle for 30 minutes before the



1 liquid was decanted. The sand was then dried at 121°C
2 overnight. A 1-kg sample of the treated sand was heated
3 to 128°C and added to a Hobart Mixer. After 30 g of
4 commercial novolak foundry resin was added to the mixer,
5 the mixture of resin and sand was blended for 90 seconds
6 to melt the resin and coat it onto the sand. Then 14.4 ml
7 of a 27.6% solution of hexamethylenetetramine in water
8 was added to the mixer. Blending was continued until the
9 mixture broke up into free-flowing grains of resin-coated
10 sand.

11
12 This procedure was repeated using Ludington,
13 Beneficiated Muskegon W/51 and Wedron 7020 silica sands.
14

15 Cold tensile and hot tensile strengths of test
16 specimens made from each of the coated sands were measured
17 as follows:

18
19 The hot tensile strengths were determined by use
20 of a Dietert No. 365 Hot Shell Tensile Tester. Tests were
21 run at 232°C with a 3-minute cure time.

22
23 The cold tensile strengths were determined by
24 making 1/4-inch thick "dog-bone" test briquets in a
25 Dietert No. 363A Heated Shell Curing Accessory. The
26 test briquets were cured for 3 minutes at 232°C and
27 allowed to cool to room temperature. The cold tensile
28
29

1 strength of each briquet was determined by using a 401
2 Universal Sand Strength Tester in the manner set forth
3 by the American Foundryman's Society.

4
5 Results of tests using the various silica sands
6 are given in Table I.
7

8 CONTROL TEST 1
9

10 The untreated sands used as starting materials
11 in Example 1 were coated with novolak resin according to
12 the procedure of Example 1. The hot and cold tensile
13 strengths of cores made from these resin-coated sands
14 were likewise tested by the procedure of that example.
15 Results of these control tests are given in Table I.
16

17 CONTROL TEST 2
18

19 Each of the sands used in Example 1 was washed
20 and dried using the same general procedure of Example 1
21 except that no sodium silicate was added to the washwater.
22 The washed sand was coated with novolak resin following
23 the procedure of Example 1, and hot and cold tensile
24 strengths were determined for cores made from these
25 resin-coated sands. Results of these control tests are
26 given in Table I.
27
28
29
30

1 These results show that impure silica lake sands
2 give foundry cores and molds with improved tensile strengths
3 if they are treated with a silicate solution before they
4 are coated with a foundry resin. In contrast, cores and
5 molds made from resin-coated, silicate-treated pure silica
6 sand show no improvement in tensile strength over those
7 prepared from untreated pure silica sand.

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1 TABLE I
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			<u>Core Properties</u>	
			Hot	Cold
			Tensile (psi)	Tensile (psi)
1	<u>Sand Type</u>	<u>Treatment</u>		
2	20KK ^{a)}	Untreated (Control Test 1)	278	400
3		Water washed (Control Test 2)	363	459
4		Silicate treated	432	525
5	Ludington ^{b)}	Untreated (Control Test 1)	190	230
6		Water washed (Control Test 2)	230	250
7		Silicate treated	335	345
8	Beneficiated Muskegon W/51 ^{c)}	Untreated (Control Test 1)	297	353
9		Water washed (Control Test 2)	284	392
10		Silicate treated	377	450
11	Wedron 7020 ^{d)}	Untreated (Control Test 1)	352	465
12		Water washed (Control Test 2)	304	500
13		Silicate treated	300	500

- 14 a) A lake sand available from the Martin Marietta Corp., Bridgman,
15 Michigan, containing about 94% SiO₂ and smaller amounts of
Al₂O₃ plus alkaline oxides and alkaline earth oxides.
- 16 b) A lake sand available from the Sargent Sand Co., Saginaw, Michigan,
17 containing 96.2% SiO₂ and smaller amounts of Fe₂O₃ and Al₂O₃ plus
18 alkaline oxides and alkaline earth oxides. The untreated sand
contained 7.3 ppm (parts per million) sodium; the silica-treated
sand contained 94 ppm sodium.
- 19 c) A washed and dried lake sand available from the Nugent Sand Co.,
20 Muskegon, Michigan, containing about 95% SiO₂ and smaller amounts
of Al₂O₃ plus alkaline oxides and alkaline earth oxides.
- 21 d) A pure silica sand available from the Martin Marietta Corp.,
22 Wedron, Illinois, containing over 99.8% SiO₂.

EXAMPLE 2

An aqueous solution of sodium silicate was prepared by adding 12.6 g of the commercially available sodium silicate solution used in Example 1 to 200 g of water. A mixture of 25.7 g of the silicate solution and 1100 g of 20KK silica sand (0.53 g sodium silicate per kg sand) was mixed in a Hobart Mixer at room temperature for 12 minutes before it was dried overnight at 232°C. One thousand grams of the treated sand was coated with 30 g of phenolic novolak resin at 128°C, and 14.4 ml of a 27.6% hexamethylenetetramine solution was added according to the procedure of Example 1. Hot and cold tensile strengths were determined for cores prepared using the resin-coated sand.

This procedure was repeated using Muskegon 850 and Vassar silica sands.

Results of the tests are reported in Table II.

For control tests, untreated 20KK, Muskegon 850 and Vassar sands were coated with phenolic novolak resin and hexamethylenetetramine solution. Hot and cold tensile strengths were then measured on cores prepared from these coated sands. The results of these control tests are also reported in Table II.

TABLE II

<u>Sand Type</u>	<u>Treatment</u>	<u>Core Properties</u>	
		<u>Hot Tensile (psi)</u>	<u>Cold Tensile (psi)</u>
20KK ^{a)}	Untreated (Control)	251	278
	Silicate treated	373	381
Muskegon 850 ^{b)}	Untreated (Control)	242	299
	Silicate treated	303	350
Vassar Sand ^{c)}	Untreated (Control)	165	215
	Silicate treated	213	257

a) A lake sand available from the Martin Marietta Corp., Bridgman, Michigan, containing about 94% SiO₂ and smaller amounts of Al₂O₃ plus alkaline oxides and alkaline earth oxides.

b) A bank sand containing about 91% SiO₂ and smaller amounts of Al₂O₃, Fe₂O₃, and alkaline oxides available from the Nugent Sand Co., Muskegon, Michigan.

c) A bank sand available from Sargent Sand Co., Saginaw, Michigan, containing about 90% SiO₂ and smaller amounts of Al₂O₃, Fe₂O₃, alkaline oxides and alkaline earth oxides.

This experiment demonstrates that silica sands can be treated with a silicate solution to give improved foundry sands and that it is unnecessary to separate the silicate solution mechanically from the treated sand.

EXAMPLE 3

Sand mixtures were prepared using various proportions of Wedron 720, a pure silica sand, and 20KK, a lake sand containing about 94% silicon dioxide. The mixtures, which contained from 96.4 to 99.6% silicon dioxide, were treated with sodium silicate solutions by the procedure of Example 2. Both treated and untreated sands were coated with novolak resin according to the procedure of Example 1. Hot and cold tensile strengths were measured on cores prepared from these coated sands. Results of these tests showed that silicate treatment is effective in improving tensile properties of cores made from sands containing less than about 99% silicon dioxide.

EXAMPLE 4

The general procedure of Example 2 was repeated with 20KK silica sand using amounts of sodium silicate varying from 0.11 to 1.79 g of sodium silicate per kg of sand. Hot and cold tensile strengths were obtained for cores prepared from silicate-treated sands which had been coated with novolak resin. These tests showed that the impure silica lake sand gave foundry cores with improved tensile strengths if the sand was first treated with between about 0.2 g and 1.1 g of sodium silicate per kg of sand.

EXAMPLE 5

In this experiment, 45.5 kg of 20KK bank sand was placed in a cement mixer. To the mixing sand was added an aqueous solution of sodium silicate prepared by mixing 63 g of the commercially available sodium silicate solution used in Example 1 with 1000 g water. Mixing was continued at room temperature for 90 seconds before a gas flame was applied to the mixture. Heating was continued until the temperature of the mixture reached 166°C. The hot treated sand was transferred to a Muller Mixer and coated with phenolic novolak resin at 128°C using the same relative proportions of resin, hexamethylenetetramine and sand as used in Example 2.

In a control experiment, untreated 20KK bank sand was heated to 180°C, transferred to a Muller Mixer and coated with phenolic novolak resin by the same procedure used to coat the treated sand.

Cores were prepared from the treated coated sand as well as from untreated coated sand which was used as a control. Hot and cold tensile strengths of the cores were measured by the standard procedures. Silicate-treated coated sand gave cores which showed a hot tensile strength of 468 psi and a cold tensile strength of 471 psi. These values compared with a hot tensile strength of 336 psi and a cold tensile strength of 362 psi for cores prepared from the untreated coated sand.

2 This experiment shows that the procedure of this
3 invention is readily scaled up to a commercially acceptable
4 process without the need for mechanical separation of the
5 silicate solution from the treated sand.

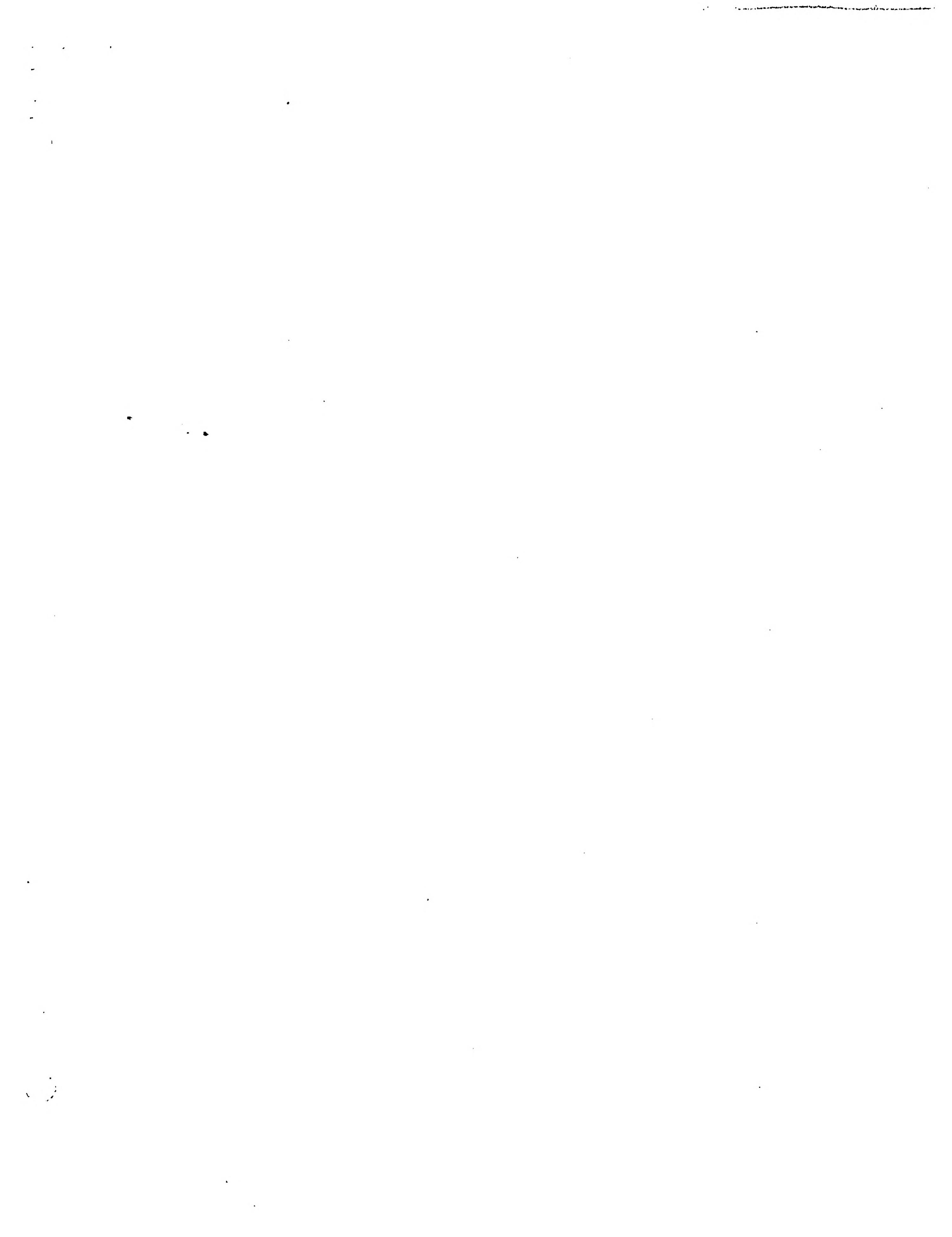
6 EXAMPLE 6

7 An aqueous solution of sodium silicate was prepared
8 by diluting 17 g of a sodium silicate solution available from
9 the Diamond Shamrock Corp. containing 6.7% Na₂O and 25.8%
10 SiO₂ with 195 g of water. This solution was used to treat
11 Vassar sand according to the procedure of Example 2 and test
12 cores were evaluated as described in that example.
13

14 Foundry cores prepared with silicate-treated sand
15 showed a hot tensile strength of 253 psi and a cold tensile
16 strength of 270 psi. These values compared with a hot
17 tensile strength of 165 psi and a cold tensile strength of
18 215 psi for the control sand which had not been treated with
19 silicate solution.
20

21 EXAMPLE 7

22 A mixture of 1000 g of 20KK silica sand, treated
23 with sodium silicate solution as in Example 2, and 30 g of
24 701 Liquid Shell Resin (a single-stage shell resin solution
25 available from the Acme Resin Corporation, Forest Park,
26
27



1 Illinois, having a pH of 3.5 to 4.5, a viscosity at 25°C of
2 3500-4500 cps and a solids content of 72% to 75% by weight)
3 was mixed in a Hobart Mixer for 3 minutes at 149°C. Then
4 14 ml of water was added to cool the coated sand and cause
5 the sand to break up into individually coated grains.
6 After the individual grains had formed, 1.2 g of calcium
7 stearate was added and mixing was continued for 1 minute.
8 Hot and cold tensile strengths of test specimens prepared
9 from the sand were determined by the procedures described
10 in Example 1. The hot tensile strength of the specimens
11 was 140 psi and the cold tensile strength was 410 psi.

12
13 Control tests performed using untreated 20KK sand
14 gave specimens showing 100 psi cold tensile and 270 psi hot
15 tensile strengths.

16
17 These results show that cores prepared using
18 silicate-treated sand coated with single-stage shell
19 resins have improved hot and cold tensile strength over
20 cores prepared from untreated impure sand.

21
22 EXAMPLE 8

23
24 This is an example of a "no-bake" foundry process.
25 Silicate-treated 20KK bank sand was prepared as in Example 5.-
26 To 2500 g of the silicate-treated sand in a K-45 Kitchen
27 Aid Mixer was added 17.2 g of Acme Bond 5022 polyol, 14.1 g
28
29

1 of Acme Bond 5062 polyisocyanate and 0.63 g of Acme Bond 5082
2 basic catalyst. The Acme Bond components are available from
3 the Acme Resin Corporation, Forest Park, Illinois. Sand and
4 resin components were mixed for 1 minute and discharged into
5 a Dietert No. 623-50 pyramid core box. The sand was jolted
6 4 times using a Dietert No. 623 core box jolter. A thermometer
7 was inserted about 6 inches into the core. The stripping
8 time is the time it takes to cure the core so hard that the
9 thermometer can no longer be pushed by hand deeper into the
10 core. Strip time was determined to be 5 minutes 15 seconds.

11
12 A second identical sand-resin mix was prepared and
13 discharged into a Dietert No. 696, 12-gang tensile core box
14 to prepare 12 standard American Foundrymen's Society 1-inch
15 dog bone tensile briquets. The cores were cured at room
16 temperature and broken after 1 hour and 24 hours. Humidity
17 testing was carried out by placing tensile briquets in 80%
18 and 90% relative humidity (r.h.) chambers for 24 hours before
19 determining tensile strengths. The tensile strengths were
20 measured using a Detroit Testing Machine Co. Model SCT Tester,
21 and scratch hardness was determined using a Dietert No. 674
22 scratch hardness tester. Results of the tests are summarized
23 in Table III.

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1 As a control, the above procedure was repeated using
2 untreated 20#K lake sand with the same amount of resin
3 components except that 0.75 g of the Acme Bond 5082 catalyst
4 was used. In this case, a strip time of 5 minutes 30 seconds
5 was obtained. Results of the other control tests are given
6 in Table III.

7 TABLE III

8

9 Cores Prepared 10 From	Tensile, psi and (Scratch Hardness)			
	11 1 hr	12 24 hrs	13 24 hrs 14 @ 80% r.h.	15 24 hrs 16 @ 90% r.h.
Treated Sand	147 (64)	267 (72)	217 (71)	157 (61)
Untreated Sand (Control)	120 (62)	183 (70)	200 (70)	123 (64)

17 These results show that cores prepared from the
18 silicate-treated sand by a base-catalyzed "no-bake" process
19 generally give improved tensile strength and better scratch
20 hardness than the cores prepared from untreated impure sand.
21 Cores prepared from treated sand also gave improved
22 release from the core box. This property is beneficial
23 because sticking to the core box slows production in a
24 foundry and can result in core or mold damage during
25 removal from the pattern.

EXAMPLE 9

A mixture of 4000 g of 20KK silica sand, treated with sodium silicate solution as in Example 2, and 40 g of powdered corn cereal was mulled in a Simpson Mix-Muller (18-inch model) for 1 minute. Then 80 g of water was added and mulling was continued for an additional 4 minutes. Mulling was stopped and 20 g of foundry core oil, obtained from the Archer-Daniels-Midland Company, Minneapolis, Minnesota, was added. The mixture was mulled for 1 minute and collected in a polyethylene bag. The bag was sealed immediately to minimize contact with the air.

Green compression strength of the coated sand was determined by placing 168 g of the material in a Dietert Detroit No. 315-9 specimen tube. The specimen was rammed three times with a Dietert Detroit No. 315 sand rammer. The resulting 2-inch x 2-inch test cylinder was compressed in a Dietert Detroit No. 465 compression instrument to determine the green compression strength.

Baked tensile strength specimens were prepared from the coated sand by placing the sand in a tensile specimen mold and ramming it four times with the Dietert Detroit No. 315 sand rammer. Specimens were placed in a tray in a circulating air oven at 224°C. Specimens were removed from the oven at varying times. After the specimens had cooled

1 to room temperature, their tensile strengths were measured
2 using a Detroit Testing Machine, Model CST, tensile tester.
3 Each value reported is the average of the strengths measured
4 using three specimens.

5
6 For comparative tests, specimens were prepared from
7 coated 20KK sand that had not been treated with silicate
8 solutions.

9
10 The results given in Table IV show that cores made
11 from silicate-treated sand coated with a core oil mix exhibit
12 about 25% greater tensile strength than do cores made from
13 uncoated sand when the cores are baked for 30 minutes.

14
15 TABLE IV

		Tests on Specimens From Silicate-Treated Sand (psi)	Control Tests (psi)
20	Green Compression	0.5	0.45
21	Baked Tensile Strength (Baking Time, min)		
22	15	60	60
23	30	225	180
24	45	215	180
25	60	235	187

1 Thus, it is apparent that there has been provided,
2 in accordance with the invention, a process for the
3 preparation of resin-coated silica sands that fully
4 satisfies the objects, aims and advantages set forth
5 above. While the invention has been described in
6 conjunction with specific embodiments thereof, it is
7 evident that many alternatives, modifications, and
8 variations will be apparent to those skilled in the
9 art in light of the foregoing description. Accordingly,
10 it is intended to include all such alternatives,
11 modifications, and variations as set forth within the
12 spirit and scope of the appended claims.

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THE EMBODIMENTS OF THE INVENTION IN WHICH AN EXCLUSIVE PROPERTY OR PRIVILEGE IS CLAIMED ARE DEFINED AS FOLLOWS:

1. A process for the preparation of treated silica sand useful for the preparation of foundry cores and molds having improved tensile strength which comprises treating impure silica sand containing from about 85% to less than about 99% of weight of silicon dioxide with a solution consisting of an alkali metal silicate and water and heating the mixture of sand and silicate to give a treated silica sand containing from about 0.2 g to about 1.1 g of silicate per kg of sand on a dry solids basis.
2. The process of claim 1 wherein the alkali metal silicate is sodium silicate.
3. The process of claim 1 wherein the impure silica sand is selected from the group consisting of 20KK lake sand, Ludington lake sand, Muskegon bank and lake sands, and Vassar bank sand.
4. The process of claim 1 wherein the silica sand is separated from the aqueous solution of an alkali metal silicate before the mixture of sand and silicate is heated.
5. A process for the preparation of a molding composition useful for forming foundry cores and molds having improved tensile strength which comprises treating impure silica sand containing from about 85% to less than about 99% by weight of silicon dioxide with a solution consisting of an alkali metal silicate and water heating the mixture of sand and silicate to give a treated silica sand containing from about 0.2 g to about 1.1 g of silicate per kg of sand on a dry solids basis, and mixing or coating the treated sand with an effective bonding amount of a binder selected from the group consisting of shell resins, base-curing "no-bake" resin components and core oil mixes.
6. The process of claim 5 wherein the alkali metal silicate is sodium silicate.

7. The process of claim 5 wherein the impure silica sand is selected from the group consisting of 20KK lake sands, Ludington lake sand, Muskegon bank and lake sands, and Vassar bank sand.
8. The process of claim 5 wherein the silica sand is separated from the aqueous solution of an alkali metal silicate before the mixture of sand and silicate is heated.
9. The process of claim 5 wherein the binder is a shell resin which further comprises the curing agent hexamethylenetetramine.
10. The process of claim 5 wherein the binder consists of "no-bake" resin components which comprise a polyol and a polyisocyanate.
11. The process of claim 10 wherein the resin components further comprise a tertiary amine.
12. The process of claim 5 wherein the binder is a core oil mix comprising a drying oil and a cereal binder.
13. A silica foundry sand useful for the preparation of foundry cores and molds having improved tensile strength prepared by treating impure silica sand containing from about 85% to less than about 99% by weight of silicon dioxide with a solution consisting of an alkali metal silicate and water and heating the mixture of sand and silicate to give a product containing from about 0.2 g to about 1.1 g of silicate per kg of sand on a dry solids basis.
14. The product of claim 13 wherein the alkali metal silicate is sodium silicate.
15. The product of claim 13 wherein the impure silica sand is selected from the group consisting of 20KK lake sand, Ludington lake sand, Muskegon bank and lake sands, and Vassar bank sand.

16. The product of claim 13 wherein the silica sand is separated from the aqueous solution of an alkali metal silicate before the mixture of sand and silicate is heated.

17. A molding composition useful for the preparation of foundry cores and molds having improved tensile strength comprising an impure silica sand containing from about 85% to less than about 99% by weight of silicon dioxide, previously treated by heating with a solution consisting of an alkali metal silicate and water to give a treated sand containing from about 0.2 g to about 1.1 g of silicate per kg of sand on a dry solids basis, and an effective bonding amount of a binder selected from the group consisting of shell resins, base-curing "no-bake" resin components and core oil mixes.

18. The composition of claim 17 wherein the alkali metal silicate is sodium silicate.

19. The composition of claim 17 wherein the impure silica sand is selected from the group consisting of 20KK lake sand, Ludington lake sand, Muskegon bank and lake sands, and Vassar bank sand.

20. The composition of claim 17 wherein the binder is a shell resin which further comprises the curing agent hexamethylenetetramine.

21. The composition of claim 17 wherein the binder consists of base-curing "no-bake" resin components which comprise a polyol and a polyisocyanate.

22. The composition of claim 21 wherein the resin components further comprise a tertiary amine.

23. The composition of claim 17 wherein the binder is a core oil mix comprising a drying oil and a cereal binder.

